

Contrast echocardiography for assessing left ventricular vortex strength in heart failure: a prospective cohort study

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Received 28 December 2012; accepted after revision 12 March 2013; online publish-ahead-of-print 14 April 2013

Aims

This study investigated the incremental role of echocardiographic-contrast particle image velocimetry (Echo-PIV) in patients with heart failure (HF) for measuring changes in left ventricular (LV) vortex strength (VS) during phases of a cardiac cycle.

Methods and results

Echo-PIV was performed in 42 patients, including 23 HF patients and 19 controls. VS was measured as a fluid-dynamic parameter that integrates blood flow rotation over a given area and correlated with non-invasively derived indices of LV mechanical performance. In comparison with early and late diastole, the VS was higher during isovolumic contraction (IC) for control and HF patients with the preserved ejection fraction (P = 0.002 and P = 0.01, respectively), but not for HF patients with the reduced ejection fraction (P = 0.41). On multivariable regression analysis, the VS during IC (VS_{IC}) was independently related to late-diastolic VS and LV longitudinal strain ($R^2 = 0.63$, P < 0.001 and P = 0.003, respectively). Patients in whom diastolic VS was augmented during IC showed a higher LV stroke volume (P = 0.01), stroke work (P = 0.02), and mechanical efficiency (P = 0.008). Over a median follow-up period of 2.9 years, eight (34%) HF patients were hospitalized for decompensated HF. In comparison with the rest, these eight patients showed markedly reduced longitudinal strain (P = 0.002), and lower change in VS (P = 0.004).

Conclusion

Our preliminary data suggest that the persistence of vortex from late diastole into IC is a haemodynamic measure of coupling between diastole and systole. The change in VS is correlated with LV mechanical performance and shows association with adverse clinical outcomes seen in HF patients.

Keywords

Particle image velocimetry • Vortex • Left ventricle • Mechanical efficiency • Heart failure

Introduction

Several numerical models, *in vitro* experiments, and imaging studies have shown that the transmitral blood flow during early-diastolic filling results in the formation of a left ventricular (LV) intracavitary vortex.^{1–8} The LV vortex has been suggested to minimize kinetic energy dissipation and reduces the total energy required for eventual ejection.^{1–8} Preliminary observations have further suggested that LV remodelling results in attenuation of the blood flow kinetic energy.⁹ Given the complexity and the number of

assumptions involved in experimental studies and relative dearth of data in humans, confirmation of proposed flow dynamics with the direct measurement of the blood flow sequence in clinical settings is crucial.

Kilner et al. ¹⁰ suggested that diastolic vortices are preserved by asymmetry of the flow paths that facilitate continued redirection of the blood flow towards the LV outflow for optimal ejection. Furthermore, the vortex formed in diastole persists into the period of isovolumic contraction (IC), which follows the mitral valve closure and is characterized by a rapid rise in LV pressure

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before opening of the aortic valve.¹¹ An organized LV intracavitary blood flow into IC may enhance coupling between diastole and systole, optimizing LV performance; however, the relationship of the LV flow to wall mechanics is a topic that has not been directly validated in clinical settings.

Echocardiographic-contrast particle image velocimetry (Echo-PIV) allows flow quantification; 12 its concept has been approve for vascular measurements and validated in accurate in vitro settings. 12-14 The feasibility of Echo-PIV for visualizing the LV flow has been recently validated 15,16 and potential applications have been verified in experimental¹¹ and clinical settings.¹⁶ For the present investigation, we hypothesized that the strength of vortex persisting from diastolic filling into IC is a haemodynamic marker, that is, associated with LV mechanical performance. The present investigation, therefore, explored the spatial and temporal characteristics of the two-dimensional (2D) blood flow in relation to LV mechanical activity in compensated heart failure (HF) patients attending outpatient clinic (ACC/AHA Stage C or D HF).¹⁷ Vortex strength (VS) was quantified as the total rotation rate of the flow in a bounded region. Asymptomatic patients with risk factors who were found to have normal LV structure and function on screening echocardiograms (ACC/AHA Stage A)¹⁷ were used as a non-HF control group.

Methods

We identified 47 consecutive subjects including 27 consecutive patients with Stage C or D compensated HF and 20 asymptomatic patients with risk factors who underwent an outpatient echocardiogram between July 2008 and July 2010 with a single provider (P.S.). The subjects were subsequently consented for an additional contrast echocardiogram. Exclusion criteria included decompensated HF, LV aneurysm, inotropic support at the time of evaluation, atrial fibrillation, hypertrophic or restrictive cardiomyopathy, pericardial diseases, valve disease (valvular stenosis or more than mild valvular regurgitation), primary pulmonary hypertension, congenital heart disease, acute coronary event or coronary artery bypass graft surgery (within 3 months), pregnancy, and patient refusal/inability to sign the informed consent form. Of the 47 patients, 5 were excluded because of suboptimal 2D or contrast echocardiographic image quality. Of the remaining 42 patients, 23 belonged to Stage C or D compensated HF with 10 patients having preserved ejection fraction (HFPEF) and 13 patients having the reduced ejection fraction (HFREF; <50%). Demographic features, risk factors, New York Heart Association class, and treatment are shown in Table 1. The institutional review board approved the study and all patients provided written informed consent.

Standard B-mode and Doppler echocardiography

Cine loops from three standard apical views (four-chamber, two-chamber, and apical long-axis) and short-axis views at the mitral valve, papillary and apical levels were recorded using greyscale harmonic imaging (Vivid 7, GE Medical Systems, Horten, Norway), following the guidelines recommended by the American Society of Echocardiography. End-diastolic and end-systolic volumes were used to calculate the ejection fraction by Simpson's biplane method from the apical four- and two-chamber views. Pulsed-wave Doppler echocardiography was performed to obtain early and late-diastolic transmitral flow velocities. Pulsed-wave tissue Doppler velocities were measured

at the septal and lateral mitral annulus in the four-chamber view and were averaged for obtaining mean early-diastolic mitral annulus velocity and the ratio of early-diastolic transmitral flow velocity to early-diastolic mitral annulus velocity. Diastolic dysfunction and its severity was described as per the published recommendations.¹⁹ We also calculated LV sphericity index,²⁰ LV stroke work,²¹ and LV mechanical efficiency (ratio of stroke work/myocardial oxygen consumption, simplified as the amount of blood pumped by a single heart beat in 1 s.^{22–25}), as per previously determined definitions.

Speckle-tracking strain echocardiography

LV subendocardial longitudinal and circumferential strain and radial strain from full thickness of the myocardium were measured (50–80 frames/s) using the 2D Cardiac Performance Analysis© software (TomTec Imaging Systems, Munich, Germany), an extended version of a previously validated software (syngo® Velocity Vector Imaging $^{\rm TM}$, Siemens Medical Solutions USA, Inc., Malvern, PA, USA). 26 Net LV twist was calculated as the net difference between LV peak rotation angles obtained from basal (CW, clockwise) and apical (CCW, counterclockwise) short-axis planes. Dyssynchrony was measured as the standard deviation of the time to minimum (for longitudinal and circumferential) or to maximum (for radial) strain obtained from 16 LV segments.

Contrast echocardiography

Two-dimensional contrast echocardiography was performed with a perfluoropropane gas-filled, lipid-stabilized microbubble (Definity®, Lantheus Medical Imaging, Inc., North Billerica, MA, USA; 0.1–0.2 mL infused intravenously as bolus injection). Two-dimensional images of the intraventricular flow were obtained from the apical long-axis view at a mechanical index of 0.1–0.4. The width and depth of the ultrasound scan area (*Figure 1*) and the spatial temporal settings were optimized to achieve the highest possible frame rates (204 \pm 39 frames/s).

Images were acquired when the bubble density and motion were optimal and best visually appreciable. On the one hand, the density of bubble had to be sufficient to appreciate their individual motion, on the other, saturation had to be avoided to make bubbles distinguishable. To verify this, we first obtained anatomical M-mode images from the 2D contrast scans along the central scanning axis as described previously (*Figure 2*).¹¹ This acquisition ensures that the same bubbles remain in the scan plane for finite period of time resulting into the formation of streaks in the dark blood pool. The presence of these streaks ensures that the bubble density is optimal for creating speckle patterns that can be tracked in the ultrasonic scan plane. Nevertheless, it was previously demonstrated theoretically²⁷ that the bubble density has only a weak influence on the results of image analysis for blood motion.

Echocardiographic particle image velocimetry

Echo-PIV uses pairs of sequential digital images for calculating the direction and magnitude of the fluid flow. 12,14,16 For this, contrast images with particles were exported into files as a stack of images during a cardiac cycle and were analysed frame by frame with a PIV software (time-resolved analysis, INSIGHTTM 3G TSI, Inc., Shoreview, MN, USA¹¹) to obtain the velocity vector field (*Figure 1*). The interrogation window of 32×64 pixels with 50% overlap was used for analysis. Maximal particle displacement was <16 pixels in *x*-axis direction and <32 pixels in *y*-axis direction during the first interrogation and adjusted until optimal Echo-PIV tracking was achieved. The reliability of the evaluated velocities that may be affected by either local

Table I. Baseline characteristics of study subjects

	Non-HF control $(n = 19)$	Heart failure			
		HFPEF (n = 10)	HFREF (n = 13)		
Age (years)	61 <u>+</u> 10	65 <u>+</u> 12	75 <u>+</u> 7 ^{*,***}	0.001	
Female gender (%)	8 (42)	3 (30)	1 (7)	0.10	
Body surface area (m ²)	1.88 ± 0.28	1.87 ± 0.20	1.98 ± 0.19	0.37	
Systolic blood pressure (mmHg)	132 ± 17	129 ± 19	135 ± 22	0.80	
Diastolic blood pressure (mmHg)	77 ± 10	70 ± 15	73 <u>+</u> 10	0.21	
Heart rate (beats/min)	67 ± 11	72 ± 19	72 ± 13	0.71	
PR (ms)	156 <u>+</u> 17	132 ± 30	142 ± 38	0.05	
QRS (ms)	88 ± 10	117 ± 29**	167 ± 40*,***	< 0.001	
QRS >120 ms (%)	1 (5)	4 (40)	11 (84)	< 0.001	
Left bundle branch block (%)	1 (5)	0 (0)	3 (23)	0.15	
NYHA class	_	1.3 ± 0.6	2.1 ± 0.9	0.02	
Risk factors (%)					
Diabetes	2 (10)	3 (30)	5 (38)	0.16	
Hypertension	10 (52)	4 (40)	9 (69)	0.36	
Hyperlipidaemia	8 (42)	4 (40)	11 (84)	0.03	
Coronary artery disease	2 (10)	1 (10)	8 (61)	0.002	
Renal failure(Cr >1.2)	0 (0)	6 (60)	5 (38)	0.37	
Medications (%)					
ACEI or ARB	1 (5)	3 (30)	10 (76)	< 0.001	
Beta blocker	4 (21)	7 (70)	11 (84)	< 0.001	
Calcium-channel blocker	2 (10)	3 (30)	1 (7)	0.25	
Digoxin	_	_	4 (30)	_	
Diuretics	2 (10)	8 (80)	8 (61)	< 0.001	

EF, ejection fraction; HFPEF, HF with preserved EF; HFREF, HF with the reduced ejection fraction; NYHA, New York Heart Association; ACEI, angiotensin-converting enzyme inhibitor; ARB, angiotensin receptor blocker.

absence or contrary excessive saturation of contrast agent is automatically monitored by the software by excluding vectors with small cross-correlation coefficient. To find subpixel displacement, we used a three-point, two-direction, Gaussian peak fitting in one dimension Illustrative figures and movies were prepared using the dedicated software (Hyperflow, Amid.net, Sulmona, Italy).

Once the velocity field was obtained, the spatial distribution of *vorticity* was computed, at every frame, using Tecplot (Tecplot, Inc., Bellevue, Washington, DC, USA). Vorticity, which corresponds to the local angular velocity of a fluid particle, represents the key quantity in fluid dynamics as it permits the delineation and quantification of vortices and shear layers. Mathematically, it is computed by taking the curl of velocity vector. Vorticity (i, j, t) was calculated by numerical derivatives.

$$\begin{split} \text{Vorticity} &= 1000 \, \times \left\{ \frac{Vy(i+1,j) - Vy(i-1,j)}{x(i+1,j) - x(i-1,j)} - \frac{Vx(i,j+1) - Vx(i,j-1)}{y(i,j+1) - y(i,j-1)} \right\} \\ &= 1000 \, \times \left(\frac{dVy}{dx} - \frac{dVx}{dy} \right). \end{split}$$

Units are as follows: x (mm), y (mm), $\forall x$ (m/s), and $\forall y$ (m/s).

Vorticity is a useful quantity to describe the underlying structure of a moving fluid. A region with compact vorticity represents a region with circular streamlines and constitutes a vortex; a region with elongated vorticity distribution exhibits a difference of velocity between the

two sides and, thus, constitutes a shear layer, which serves as a boundary layer in vicinity of the wall. A brief introduction of the role vorticity for the cardiac flow has been recently reviewed²⁸; and a more in-depth discussion on the same topic can be found elsewhere.²⁹

In integral terms, vorticity defines the amount of circulatory (swirling) fluid dynamics. To evaluate such a feature of the motion, vorticity distribution was plotted in the form of a histogram based on the percentage of the map area vs. the vorticity values ω (s⁻¹) throughout the entire flow map (*Figure 3*). Based on conventions, CCW and CW vorticity are represented in red and blue, respectively, on the contour map.

Following the procedure outlined in *Figure 3*, we further characterized the amount of CW and CCW swirl by the circulation, that is, computed by taking the product of the corresponding mean vorticity and the area occupied by such vorticity within the area enclosed by the scanned image boundary. VS refers to the total amount of swirl (or circulation), and was calculated by summing up the value of the both the CW and the CCW values of the circulation. Early and late diastole and IC periods were delineated as previously described¹¹ and average VS was calculated during each of these three periods.

 VS_{IC} was considered augmented if the magnitude was greater than the VS attained during early or late diastole (VS_E or VS_A). We also calculated the absolute change in VS from early diastole to IC and expressed it as a fractional change in VS from early diastole to IC ($[VS_{IC} - VS_E]/VS_{IC}$).

 $^{^*}P$ < 0.05 non-HF control vs. HFREF.

 $^{^{**}}P$ < 0.05 non-HF control vs. HFPEF.

^{****}P < 0.05 HFPEF vs. HFREF.

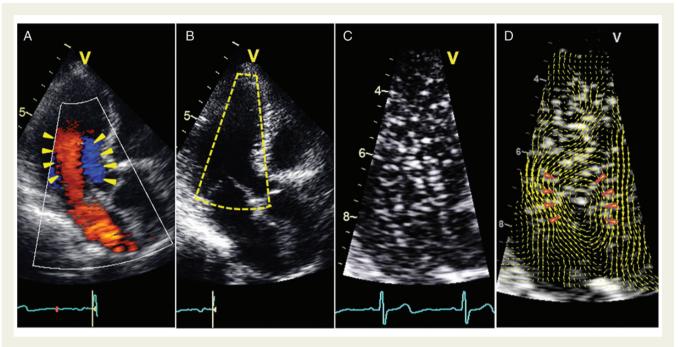


Figure 1. Echocardiographic-contrast particle imaging velocimetry. (A) Colour Doppler imaging showing the bidirectional flow during early diastole. (B) Delineation of the region of interest in the submitral and LV outflow region. (C) High-temporal resolution contrast echocardiography is performed for the region of interest. (D) Contrast particle imaging velocimetry shows the flow field with velocity vectors. Note the presence of a CW vortex (arrows).

Follow-up

Observed survival was assessed through a search of medical records and the Social Security Death Index on 1 November 2011. Rehospitalization for decompensated HF and all-cause mortality was recorded for each of the 23 HF patients from the date of echocar-diography through November 2011, resulting in a median length of follow-up of 2.9 years. The following clinical events were reported as endpoints: cardiac death, hospitalization due to cardiac decompensation, or necessity for heart transplantation. The first event that occurred was used for the analysis.

Statistical analysis

Statistical analysis was performed with commercially available software (MedCalc 11.2, MedCalc Software, Mariakerke, Belgium). All continuous data were reported as means \pm standard deviation, and categorical data as percentages. The Kruskal-Wallis test was used for non-parametric comparisons among independent non-HF control and HF groups and the Friedman test was used for nonparametric comparisons of repeated measurements of VS among cardiac cycle phases. The Mann-Whitney U-test was used for non-parametric comparisons of unpaired measurements between non-HF control and/or HF groups and the Wilcoxon rank-sum test was used for non-parametric comparisons of paired measurements of VS between cardiac cycle phases. The χ^2 test was used for comparisons of categorical variables. Univariate and multivariate linear regression analysis was performed to determine correlates of VS_{IC}. Statistical significance was defined as a two-tailed P-value < 0.05. Intra-observer and inter-observer variability for the measurement of VS were calculated as means \pm standard deviations of percentage ratios between absolute differences and means of the two independently measured variables in 10 randomly selected patients. Inter-observer agreement and

intra-observer consistency were assessed with the Bland–Altman analysis. 30

Results

Clinical characteristics

Differences in baseline clinical and echocardiographic characteristics for HF patients and non-HF controls are shown in Tables 1 and 2, respectively. HFREF patients were older (P = 0.001) with a higher prevalence of coronary artery disease (P = 0.002) and prolongation of QRS interval on surface electrocardiogram (P <0.001). On echocardiography, HFREF patients showed significantly larger left atrial volume (P = 0.004), greater LV remodelling with the increased LV dimensions and sphericity index (P < 0.001 for each), and significantly increased ratio of the early-diastolic flow to mitral annular lengthening velocity (P = 0.001; Table 2). In comparison with non-HF controls and HFPEF, global LV strains in longitudinal, circumferential and radial directions, and net twist were significantly reduced in HFREF patients (P < 0.05 for each). Similarly, in comparison with non-HF controls and HFPEF, HFREF patients showed the presence of significant dyssynchrony in the longitudinal direction (P = 0.01).

LV fluid dynamics

For non-HF control, both VS_E and VS_A were similar in magnitude; however, the magnitude of VS_{IC} was significantly higher than VS_E and VS_A (P=0.01 vs. and 0.002, respectively). Although VS_E in patients with HFPEF was lower than in non-HF controls (P=0.09) and not different from VS_A, the magnitude of VS_{IC}

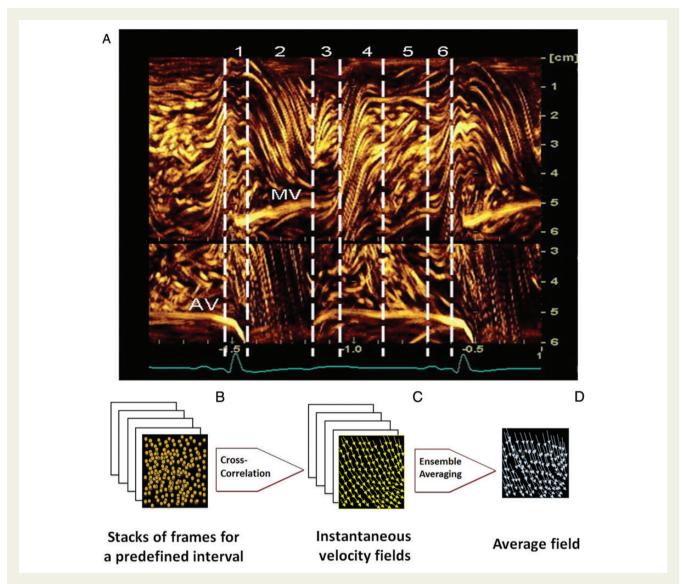


Figure 2. Assessment of LV intracavitary flow, contrast density, and motion. (A) An anatomical M-mode through the LV cavity during contrast infusion. The axial movement of contrast bubbles produces bright streaks, which suggest optimum contrast density and temporal resolution for tracking. The phases of cardiac cycle are then determined using the movement of the MV and the AV. Phases: 1, pre-ejection; 2, ejection; 3, isovolumic relaxation; 4, early diastole; 5, diastasis; and 6, late diastole. (B) Series of phase locked image frames are obtained during time intervals through the cardiac cycle as defined above. (C) Sequential pairs of these frames are cross-correlated for obtaining the velocity vectors. (D) Ensemble average of the sequential vector fields obtained for each time interval defines the dominant flow features in the flow field for that specific time interval.

was augmented and higher than VS_A (P=0.01). In contrast, for patients with HFREF, VS_E was not significantly different than in non-HF controls, however, VS_{IC} failed to augment to a value higher than VS_E or VS_A (Table 2 and Figures 4 and 5).

To understand the factors that contribute to VS_{IC} , we examined the univariate relationships between VS_{IC} and LV muscle and fluid mechanics variables (*Table 3*). On multivariable regression analysis, the magnitude of VS_{IC} was independently related to VS_E and LV longitudinal strain ($R^2 = 0.63$, P < 0.001). Similarly, the presence of dyssynchrony in the longitudinal strain was associated with VS_{IC} in HF patients (r = -0.54, P = 0.04). Supplementary data online, *Movies S1* and *S2* show a non-HF control

subject with VS, that is, higher in IC, whereas Supplementary data online, Movies S3 and S4 illustrate an example of attenuated VS_{IC} in a patient with HFREF. The presence of greater VS_{IC} than the highest VS recorded during the diastolic phases was associated with a higher LV stroke volume (odds ratio: 1.09; confidence interval: 1.02–1.17; P=0.011), stroke work (odds ratio: 1.03; confidence interval: 1.00–1.06; P=0.02), and LV mechanical efficiency (odds ratio: 1.05; confidence interval: 1.01–1.10; P=0.008). LV mechanical efficiency was related to longitudinal strain (r=0.38, P=0.05), radial strain (r=0.45, P=0.005), net LV twist (r=0.34, P=0.02), and VS change (r=0.38, P=0.01).

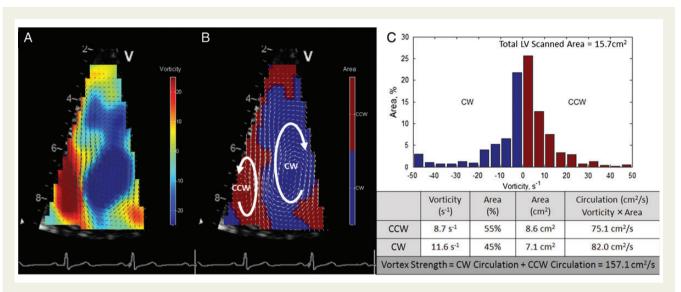


Figure 3. Calculation of circulation as a measure of VS. (A) Ensemble averaged vorticity distribution during early diastole. (B) Flow areas are separated into regions with CCW (red colour) and CW (blue colour) vorticity. (C) A histogram of CCW (positive vorticity) and CW (negative vorticity) is weighted by the percentage of area that takes such a value. Thus, the mean value of the positive and the negative vorticity is evaluated and the percentage of the corresponding areas is evaluated by summing up the histogram bins. The VS is computed by adding the circulation in CW and CCW directions (circulation is obtained by multiplying the mean vorticity with the corresponding areas).

Clinical follow-up and adverse events

Follow-up data were analysed in HF patients over a median follow-up period of 2.9 years. Of 23 patients, eight (34%) were hospitalized for decompensated HF, five (21%) patients died, and 1 patient underwent cardiac transplantation. Patients who reached an endpoint of death or hospitalization for HF (n=8) showed a lower ejection fraction (P=0.08) than remaining of the HF patients; however, had similar LA volumes and diastolic dysfunction. Patients with endpoints showed significantly lower longitudinal strain (P=0.002), circumferential strain (P=0.04), radial strain (P=0.02), and lower change in VS (P=0.004). The difference in VS change between the two groups persisted even after adjusting for the differences in LV EF (P=0.03) $(Table\ 4)$.

Inter-observer and intra-observer variability

The inter-observer and intra-observer variability for VS measurements were 7.7 ± 7.9 and $7.3\pm7.8\%$, respectively. Bland–Altman analysis was used to assess inter-observer agreement and intra-observer consistency. Mean values, their differences, and the intraclass correlation coefficients are shown in Supplementary data online, *Table S1*. VS had good reproducibility with intraclass correlation coefficients \geq 0.95 for most evaluations.

Discussion

This is the first prospective study that has (i) tested the phasic changes in the strength of intraventricular flow rotation (VS) in HF patients, using a fluid-dynamic variable computed through a

high-temporal resolution Echo-PIV, which permits flow characterization during the phases of the cardiac cycle including the brief isovolumic phases, (ii) correlated the change in VS with non-invasively derived markers of LV systolic and diastolic performance including LV deformation and twist mechanics, and (iii) provided preliminary data regarding the change in VS from early diastole to IC in patients with HF with normal or reduced ejection fraction with further follow-up over a median period of 2.9 years for characterizing the potential prognostic value of change in VS.

VS during phases of cardiac cycle

A vortex develops in the form of a shear layer adjacent to the tissue (boundary layer). When the shear layer separates from the wall, fluid tends to curl into a vortex.²⁹ Previous investigations have studied the transmitral vortex formation using numerical or physical models or through flow visualization techniques such as cardiac magnetic resonance, 2,10,31-33 colour Doppler and contrast echocardiography. 11,16,34 The LV vortex characteristics in previous studies, however, have been primarily related to the diastolic filling phases of the cardiac cycle. ^{2-5,31,35} In an experimental model, we described the persistence of the LV vortex in early systole during the IC period; however, the relation between vortex during IC and LV mechanical activity was not previously assessed. 11 In a subsequent investigation, we also reported a close coupling of LV latediastolic and IC mechanical activity and its utility in predicting peak oxygen consumption during exercise.³⁶ The present investigation further demonstrates the mechanical continuum of late-diastolic and IC phases of the cardiac cycle. A circulating blood flow during late diastole is smoothly continued into the phase of IC; where it becomes the eventual outcome of the diastolic vortex formation process that can relate with the LV mechanical activity

Table 2. Echocardiographic variables of study subjects

	Control $(n = 19)$	Heart failure		
		HFPEF (n = 10)	HFREF (n = 13)	
Standard echocardiography				
LV septum (mm)	9 <u>+</u> 1	11 <u>+</u> 2	10 ± 2	0.11
LV posterior wall (mm)	9 <u>+</u> 1	11 <u>+</u> 2	10 ± 2	0.35
LV end-diastolic dimension (mm)	45 <u>+</u> 6	44 <u>+</u> 4	62 ± 7*,***	< 0.001
LV end-systolic dimension (mm)	30 <u>+</u> 4	29 ± 4	52 ± 9*,***	< 0.001
LVEF (%)	63 ± 5	61 ± 7	28 ± 10*,***	< 0.001
LV EDV (mL)	114 <u>+</u> 40	113 ± 33	$202 \pm 79^{*,***}$	< 0.001
LV ESV (mL)	41 ± 22	43 ± 17	146 ± 76*,***	< 0.001
LVEF (%)	63 ± 5	61 <u>+</u> 7	28 ± 10*,***	< 0.001
Indexed LA volume (mL/m²)	32 <u>+</u> 9	43 ± 12**	48 ± 21*	0.004
E velocity (m/s)	0.74 ± 0.12	0.80 ± 0.29	0.80 ± 0.26	0.98
E/A ratio	1.1 ± 0.3	1.5 ± 0.6	1.7 <u>+</u> 1.5	0.13
E/e' mean	9.5 ± 3.1	13.3 ± 7.2**	22.5 ± 12.4*	0.001
Normal diastolic function (%)	14 (63)	_	_	_
Diastolic dysfunction (%)	5 (26)	10 (100)	13 (100)	< 0.001
Grade I (%)	5 (26)	2 (20)	4 (31)	
Grade II (%)	_	7 (70)	4 (31)	
Grade III (%)	_	1 (10)	5 (38)	
RVSP (mmHg)	28 ± 5	39 ± 11**	42 ± 15*	0.007
LV sphericity index	0.54 ± 0.05	0.54 ± 0.05	0.65 ± 0.09*,***	< 0.001
LV stroke volume (mL)	73 <u>+</u> 19	70 ± 22	56 <u>+</u> 14	0.08
LV stroke work (g)	119 <u>+</u> 42	110 ± 43	90 ± 26	0.30
LV mechanical efficiency (mL/s)	69 ± 28	63 ± 26	49 <u>+</u> 19	0.16
Strain, twist, and dyssynchrony				
Ls (%)	-18.3 ± 4.4	-15.2 ± 5.8	$-9.8 \pm 5.2^{*,***}$	< 0.001
Cs (%)	-23.8 ± 4.6	-22.6 ± 7.4	$-11.2 \pm 6.1^{*,***}$	< 0.001
Rs (%)	24.6 ± 9.6	19.7 ± 11.6	8.7 ± 5.2*,***	< 0.001
Net twist (degree)	10.9 ± 5.6	11.7 ± 9.2	5.5 ± 3.6*	0.02
SD of time to Ls (ms)	50 ± 21	49 ± 23	81 ± 27*	0.01
SD of time to Cs (ms)	83 ± 31	69 ± 38	82 ± 40	0.61
SD of time to Rs (ms)	126 ± 47	116 ± 44	165 ± 63	0.17
Echocardiographic PIV				
VS_F (cm ² /s)	184 ± 57	143 ± 67	182 ± 67	0.19
VS _A (cm ² /s)	_ 184 <u>+</u> 67	143 ± 47		0.15
VS_{IC} (cm ² /s)	231 ± 85*******	195 ± 103*****	203 ± 88	0.24
VS change	0.12 ± 0.33	0.21 ± 0.33	0.06 ± 0.24	0.37

LV, left ventricular; EF, ejection fraction; EDV, end-diastolic volume; ESV, end-systolic volume; LA, left atrium; E, early diastole; A, late diastole; E/e', ratio of early-diastolic transmitral flow velocity to early-diastolic tissue velocity; RVSP, right ventricular systolic pressure; Ls, longitudinal strain; Cs, circumferential strain; Rs, radial strain; PIV, particle imaging velocimetry; VS_{IC}, vortex strength during isovolumic contraction; VS_E, vortex strength in early diastole; VS_A, vortex strength in late diastole; SD, standard deviation. $^*P < 0.05$ control vs. HFREF.

in systole. This suggests a potential role of IC vortex in optimizing diastolic-to-systolic mechanical coupling.

VS in HF

During the IC period, shortening of early activated regions of LV is accompanied with stretching of the late activated regions. ^{37,38} This

reshaping deformation suggests interactions between the blood flow sequence and the LV mechanical activity developing in early systole.³⁹ Indeed, structural and functional remodelling of the LV results in an unfavourable mechanoenergetic profile (i.e. diminished mechanical efficiency)⁴⁰ and this change in mechanical efficiency may be related to the attenuation of the kinetic energy

^{**}P < 0.05 control vs. HFPEF.

^{****}P < 0.05 HFPEF vs. HFREF.

^{*****}P < 0.05 VS_{IC} vs. VS_E.

 $^{^{*****}}P$ < 0.05 VS_{IC} vs. VS_A.

of the diastolic LV flow.⁹ Furthermore, a reduction in VS, during the IC period, may alter contractility of activated myocytes due to variations in preload that influence the steepness of the Frank–Starling relationship.³⁹ These novel insights, which link LV geometry, muscle, and fluid mechanics, raise several interesting hypotheses that require further verification.

Methodological considerations

The Echo-PIV technique has been previously validated in the laminar flow⁴¹ and in the carotid bifurcation¹⁴ with good agreement seen with optical particle imaging velocimetry for *in vitro* models of the pulsatile flow.^{15,16}. However, the feasibility of using Echo-PIV in routine hospital settings for 2D contrast echocardiography for LV cavity opacification has not been sufficiently clarified. A recent

experimental study assessed Echo-PIV accuracy against optical PIV for LV flow visualization and revealed a tendency to underestimate the higher velocity when traditional clinical settings were used (frame rate < 100 Hz). We attempted to circumvent some of these limitations by using lower contrast particle density for optimal PIV tracking and using a much higher temporal resolution (frame rate: 129–252 Hz). Moreover, previous works that used Echo-PIV in clinics, or in a validation study, employed different parameters because the frame rates were insufficient for quantitatively evaluating velocities values and parameters were designed merely as a statistical measure of the overall flow pattern. The technique employed here presents, instead, a sufficient acquisition frame rate that allowed evaluating actual fluid-dynamics quantities that were further related with LV muscle mechanics.

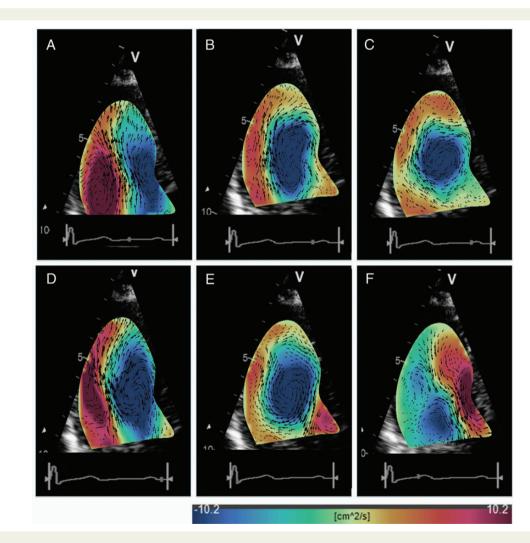


Figure 4. The LV flow sequence during phases of cardiac cycles in a non-HF control subject. LV intracavitary planar vorticity maps of a non-HF control subject (EF 61%) during phases of cardiac cycle are shown in (A-F). Note that the presence of initial CW (blue) and CCW (red) vortex during early-diastolic filling (A). The counterclockiwise flow (red) becomes weaker (B) resulting into predominantly CW (blue) vortex during the phase of diastasis (C). The atrial flow in late diastole is characterized by an increase in the strength of the CW vortex (D), which persists further during IC (E). Ejection is characterized by accelerating flow towards the LV outflow surrounded by CW and CCW shear layers (F). Movies corresponding to Figure 3 can be viewed as Supplementary data online, *Movies* S1 and S2.

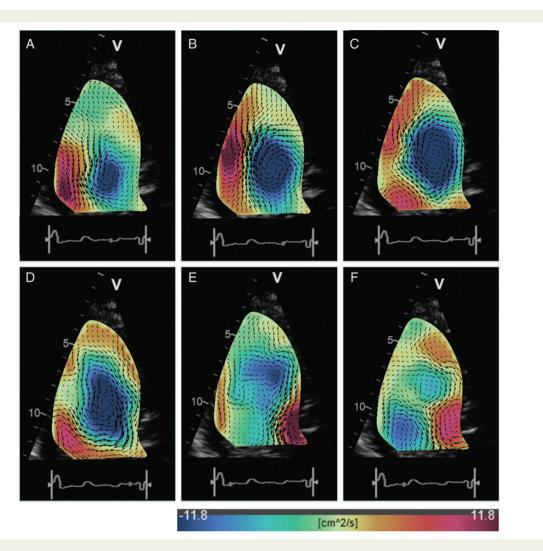


Figure 5. The LV flow sequence in HFREF. LV intracavitary planar vorticity maps of a Stage C HFREF patient (EF 34%) during phases of the cardiac cycle are shown in (A-F). The cardiac cycle (A-F) is the same as outlined in Figure 3. Note that the CW vortex is attenuated during IC (E). Movies corresponding to Figure 4 can be viewed as Supplementary data online, *Movies* S3 and S4.

Clinical significance

Clinical investigators have recently debated the binary view to HF using the terms systolic and diastolic ${\sf HF.}^{42}$ These data would support the recent suggestions that properties of failing hearts should be considered at different hierarchical scales of performance for understanding the levels of mechanical inefficiencies rather than merely relegating to binary divisions of systolic and diastolic dysfunction.⁴² Such integrative analysis of levels of energetic inefficiencies in a failing heart may provide a logical approach to characterizing multidimensional complex interactions between biomarkers in HF syndromes.⁴³ Although attempts at energetic efficiency of the blood flow were recently measured using the MRI-based assessment of blood flow fields, 44 Echo-PIV is an extension of the LV opacification technique and can be performed in minutes from LV contrast opacification, which is frequently used in HF patients. 45 Another advantage of Echo-PIV is the hightemporal resolution, which permits tracking the blood flow

sequence during the transient isovolumic phases of the cardiac cycle. Therefore, the development of echocardiographic techniques for flow visualization has potential for providing a practical technique for characterizing the degree of flow inefficiency in HF patients in clinical practice.

Study limitations

We used apical long-axis views for focusing on the dominant flow structures in the inflow and the outflow regions of the LV. Use of a full 3D structure of flow with incorporation of boundaries would be necessary for more complete assessment of the LV flow structure. The relationships between VS and the ventricle's mechanical performance shown in this investigation also need cautious interpretation. First, the VS alone may not account for other aspects, like the vortex position and its shape with respect to the LV chamber, which may play a role in the flow arrangement and influence LV performance. Furthermore, the formula used for calculating LV

Table 3. Univariate and multivariate linear regression analysis for correlates of VS during IC

	Univariate regression		Multivaria	Multivariate regression			
	Correlation	<i>P</i> -value	В	SE	t-value	P-value	R²
VS _A (cm ² /s)	0.70	< 0.001	0.75	0.10	7.31	< 0.001	0.6
VS _E (cm ² /s)	0.57	< 0.001					
Ls (%)	-0.34	0.02	-4.44	1.41	-3.14	0.003	
Cs (%)	-0.25	0.10					
Rs (%)	0.28	0.06					
Net twist (degree)	0.30	0.05					

VSA, vortex strength during late diastole; VSE, vortex strength during early diastole; Ls, longitudinal strain; Cs, circumferential strain; Rs, radial strain.

Table 4. Clinical and echocardiographic features of HF patients with and without adverse clinical events during follow-up

	Heart failure		P-value	
	Without events (n = 15)	With events $(n = 8)$		
Age (years)	71 <u>±</u> 11	71 <u>+</u> 9	0.97	
Female gender (%)	4 (30)	_	0.30	
HFPEF (n) (%)	7 (46)	3 (37)	0.98	
Standard echocardiography				
LV septum (mm)	11 ± 2	10 ± 2	0.60	
LV end-diastolic dimension (mm)	52 <u>+</u> 7	58 ± 15	0.27	
LV end-systolic dimension (mm)	39 ± 10	50 ± 16	0.12	
LVEF (%)	47 ± 16	34 ± 21	0.08	
Indexed LA volume (mL/m²)	46 ± 21	46 ± 8	0.49	
E/A ratio	1.3 ± 0.5	2.2 ± 1.7	0.14	
E/e' mean	14.7 ± 6.5	24.7 ± 14.0	0.10	
RVSP (mmHg)	40 ± 10	44 ± 18	0.75	
LV sphericity index	0.66 ± 0.15	0.72 ± 0.15	0.39	
LV stroke volume (mL)	65 ± 18	59 ± 21	0.63	
LV stroke work (g)	101 ± 31	83 ± 29	0.21	
LV mechanical efficiency (mL/s)	61 ± 23	46 ± 22	0.26	
Global strains and twist				
Ls (%)	-14.6 ± 4.6	-7.6 ± 5.9	0.002	
Cs (%)	-19.0 ± 8.2	-10.9 ± 7.4	0.04	
Rs (%)	15.9 \pm 9.7	9.0 ± 9.6	0.02	
Net twist (degree)	9.5 ± 8.1	5.7 ± 4.3	0.20	
Echocardiographic PIV				
VS_E (cm ² /s)	143 <u>+</u> 67	182 ± 67	0.29	
VS_A (cm ² /s)	192 ± 117	155 ± 40	0.54	
VS_{IC} (cm ² /s)	219 ± 108	162 ± 32	0.42	
VS change	0.24 ± 0.24	-0.08 ± 0.24	0.004	

Abbreviations are similar as in Table 2.

mechanical efficiency was simplified as the ratio between stroke volume and heart rate. Although this has been shown to provide useful information, ^{22–25} this theoretical approach differs from previous equations where energy consumption is determined by coronary

sinus catheterization to measure real-time myocardial oxygen consumption. Finally, although the difference in VS was associated with adverse cardiac events, the number of events was small and precluded a detailed survival analysis.

Conclusions

The present study establishes the sequence in which LV vortices formed during diastolic filling phases are sustained into IC for the optimal onset of ejection. Our data suggest that the persistence of VS from late diastole into IC is a marker of the fluid-continuum of the cardiac cycle and helps coupling diastole to systole without any intervening periods of haemodynamic stasis. The change in VS is correlated with LV mechanical performance and may have prognostic value for HF patients.

Supplementary data

Supplementary data are available at European Heart Journal – Cardiovascular Imaging online.

Funding

This study was supported by an intramural fund (CR-5) from Mayo Clinic, Scottsdale, AZ, USA.

Conflict of interest: none declared.

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IMAGE FOCUS

doi:10.1093/ehjci/jet095 Online publish-ahead-of-print 18 May 2013

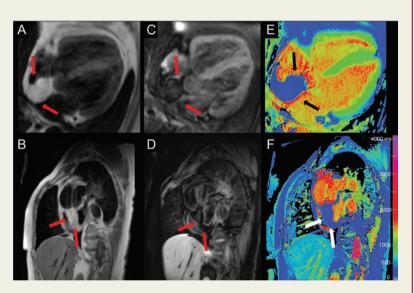
Is it really fat? Ask a T1-map

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A 67-year-old woman initially presented with dyspnoea. Echocardiography demonstrated an inter-atrial mass. Cardiovascular magnetic resonance (CMR) showed a well-marginated mass $(35 \text{ mm} \times 45 \text{ mm})$ in the inter-atrial septum (IAS) sparing the fossa ovalis, extending to the posterior right atrial wall. The mass had high signal intensity on T1-weighted images (Panels A and B, arrows) consistent with fat, which attenuated on fat-suppression imaging (Panels C and D, arrows). Native T1-maps (Panels E and F, arrows) showed homogenous and significantly lower T1 values (230-350 ms) compared with the normal myocardium (green) and blood (yellow/red), but similar to subcutaneous and epicardial fat (blue). The mass had no late gadolinium enhancement and was stable in the size



compared with 1-year prior. Findings were consistent with lipomatous hypertrophy of the IAS.

This is a first demonstration of using native T1-mapping for immediate visual and quantitative tissue characterization of an intracardiac mass to help confirm its fat content. T1-maps provide pixel-wise estimates of the T1 relaxation times of the underlying tissue, and each tissue type exhibits a characteristic normal range of T1 values. This allows the visual differentiation of tissues using colour scales as shown. Lipomatous hypertrophy of the IAS is an unencapsulated proliferation of adipose tissue ≥ 20 mm within the atrial septum that is in continuity with epicardial fat. It is associated with older age, increased fat elsewhere in the body, atrial arrhythmias and in some cases, obstruction of the superior vena cava. The correct differentiation of this benign cardiac mass from other atrial tumours using multi-parametric tissue characterization techniques on CMR can prevent unnecessary invasive interventions.

Funding

Funding to pay the Open Access publication charges for this article was provided by the Division of Cardiovascular Medicine, Radcliffe Department of Medicine, University of Oxford.

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